

Investigation on flow of Efficient Heat Flow by Compact types Heat Exchanger- A Review

¹Vishal Srivastava, ²Dr.Sohail Bux

¹M. Tech Scholar, ²Professor

¹Department of Mechanical Engineering, Agnos College of Technology Bhopal, (M.P.)

²Department of Mechanical Engineering, Agnos College of Technology Bhopal, (M.P.)

Email:- ¹vishal1912@gmail.com, ²buxsohail@gmail.com

Abstract:- The available platefin heat exchanger has rectangular offset strip geometry and is tested in the laboratory using the heat exchanger test rig. The experiment is conducted under balanced condition i.e. the mass flow rate for both sides of fluid stream is same, and the experiment is carried out at different mass flow rates. The effectiveness of heat exchanger is found out for different mass flow rates. Various correlations are available in the literature for estimation of heat transfer and flow friction characteristics of the platefin heat exchanger, so the various performance parameters like effectiveness, heat transfer coefficient and pressure drop obtained through experiments is compared with the values obtained from the different correlations. The longitudinal heat conduction through walls decreases the heat exchanger effectiveness, especially of cryogenic heat exchangers, so the effectiveness and overall heat transfer coefficient is found out by considering the effect of longitudinal heat conduction using the Kroeger's equation.

Keywords: Efficient Heat Flow, Compact types Heat Exchanger, COP.

I. INTRODUCTION

Heat exchangers are gadgets intended to move heat starting with one liquid then onto the next, without the liquids coming into contact. There is a wide assortment of uses for heat exchangers, for instance: radiators, cooling and power plants.[1]

1.1 TYPES OF HEAT EXCHANGERS

The basic design of a heat exchanger is based on the paths its streams take. Parallel stream and cross stream heat exchangers are the two most common types. Also, in certain businesses, you'll find regenerative heat exchangers.[2]

1.1.1 In Line Exchanger:

In inline exchangers, the hot and cold liquids move corresponding to one another. Heat exchangers where the liquids move in a similar course are alluded to as resemble stream or co-current, exchangers (displayed in fig.1) where liquids move the other way are alluded to as counter stream or counter-current (displayed in fig. 2)

Counter stream heat exchangers (displayed in fig.1) are innately more proficient than equal stream heat exchangers since they make a more uniform temperature contrast between the liquids, over the whole length of the liquid way. Counter stream heat exchangers can permit the "cool" liquid

to exit with a higher temperature than the leaving "hot" liquid. Anyway numerous modern hotness exchangers are more intricate. To save space, liquids might go to the furthest limit of a unit then, at that point, return once more, maybe a few times. Each time a liquid maneuvers through the length is known as a pass. For instance, one liquid might make 2 passes, the other 4 passes. Consequently parts of the hotness exchanger might be co-current, others counter-current, and estimations should consider this.[3]

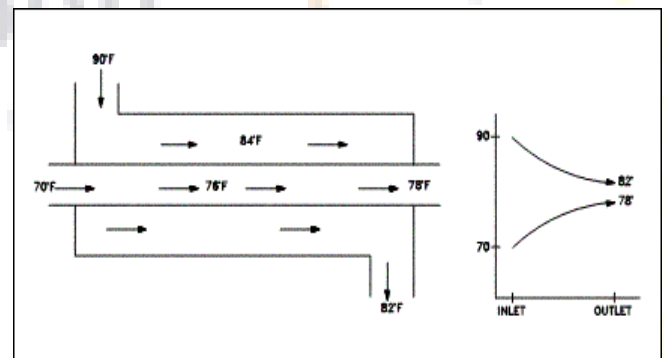


Fig.1 Inline exchanger

In Parallel stream heat exchangers, the power source temperature of the "cool" liquid can never surpass the power source temperature of the "hot" liquid.

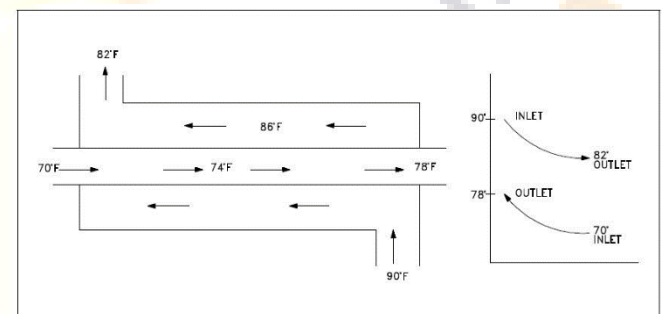


Fig.1.2 Heat exchanger with counter flow

1.2.2 Cross Flow Heat Exchanger

In cross stream exchangers, the hot and cold liquids move opposite to one another as displayed in fig. 3. This is regularly a helpful approach to genuinely find the bay and outlet ports in a little bundle, nonetheless, it is less thermally productive than an absolutely counter stream plan. Thermodynamically the adequacy of cross stream heat exchanger is fall in the middle of that for counter stream and equal stream heat

exchangers. Logarithmic mean temperature distinction (LMTD) will be more noteworthy all of the time for counter stream contrast with equal stream heat exchanger. For a given stream rate and at given channel, outlet temperatures, an equal stream heat exchanger requires greatest stream region while a counter stream heat exchanger requires least stream region and a cross stream heat exchanger region lies between two outrageous cutoff. Hence equal stream heat exchanger not utilized practically speaking and counter stream course of action is liked. Nonetheless, cross stream course of action is usually utilized in light of the fact that it is simpler to furnish delta and outlet header associations with cross stream as opposed to countering stream. Cross stream heat exchanger give smaller plan of hotness exchanger.[4]

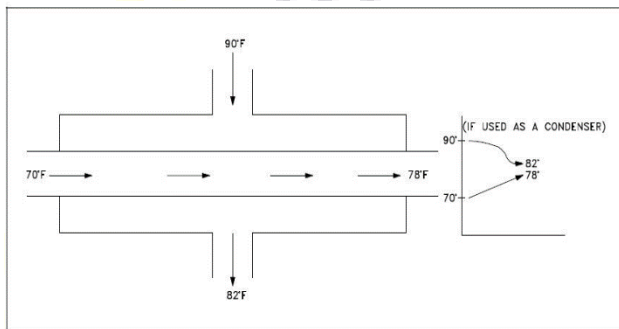


Fig.1.3 Heat exchanger with cross flow

1.2.3 Regenerative Heat Exchangers

Regenerative hotness exchangers store hotness and delivery it later. They contain a huge mass of material which doesn't leave the exchanger yet warms up (or now and again, liquefies, engrossing inactive hotness) as hot liquid is gone through. In this way heat from one clump activity can be utilized to heat up the following one. Then again, they can be utilized two by (at least two) with one engrossing hotness from a hot stream while the other is releasing it to a virus stream. In certain plans the bed of hotness engrossing material moves to convey heat starting with one stream then onto the next.[5]

The term regenerative hotness exchanger is likewise utilized for counter-stream exchangers in which one side is liquid entering the cycle and the opposite side liquid leaving the interaction.

The LMTD is a logarithmic normal of the temperature contrast between the hot and cold feeds at each finish of the twofold line exchanger. The bigger the LMTD, the more hotness is moved. The utilization of the LMTD emerges clearly from the investigation of a hotness exchanger with consistent stream rate and liquid warm properties. Fig. 1.4 shows the Temp-diagram of the hot and cold liquids along the Heat Exchanger.[6]

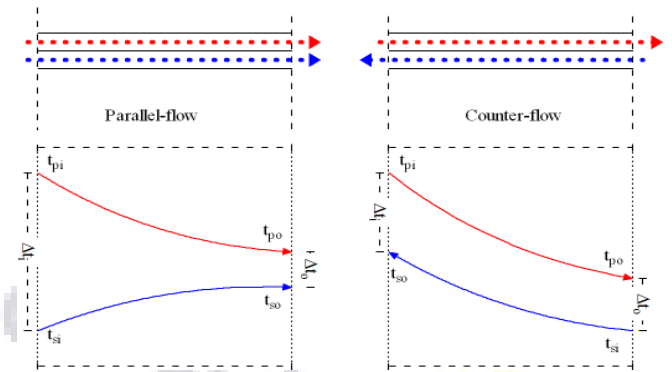


Fig.1.4 Heat exchanger with LMTD

1.3 HEAT EXCHANGER SIZING AND LMTD:

One thing to think about while estimating a hotness exchanger is the temperature contrast of the liquids we wish to utilize. While heat exchangers work effectively at moving energy, they are restricted by the hotness source or hotness sink we give them. Regardless of how enormous a hotness exchanger is made for our cycle, it can't surpass the cooling or warming given by the utility.[7]

Counter-Current Flow

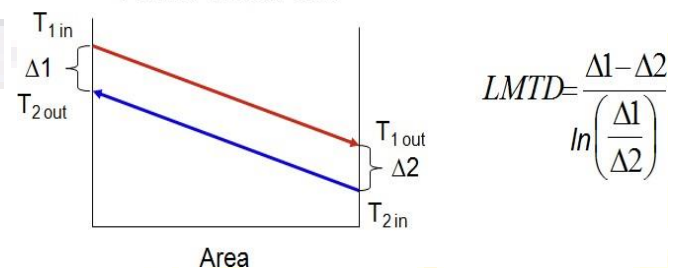


Fig.1.5 Heat Exchanger Sizing and LMTD

The above graph (in Fig. 1.5) is a typical temperature-area bend for a counter-current (Cross stream) heat exchanger. The hot liquid would enter on the "left" finish of the exchanger at its most noteworthy temperature, and cool down as it arrives at the Cold Side Inlet. The chilly liquid enters from the "right" and warms up as it trades its energy with a temperature expanding hot source, moving toward the most noteworthy temperature of the Hot Side Inlet. In the event that the two liquids at any point arrived at an equivalent temperature, the hotness move would quit that point on. Counter-current plans forestall a temperature squeeze as well as lessen the size of the hotness exchanger. The condition for the hotness load "Q" (Btu/hr) done by a framework is $Q = U \cdot A \cdot LMTD$. "U" would be the general hotness move coefficient for the cycle, "A" future the surface region, and "LMTD" is the log mean temperature distinction. The simplest method for taking a gander at the LMTD is as a correlation of the two liquid's temperatures all through the exchanger. Since most exchangers are counter-current, looking at one or the flip side of the exchanger gives a worked on illustration of the LMTD. This would be the hot outlet and cold bay, or the chilly outlet and hot channel. Assuming an interaction has an enormous LMTD (meaning your as of late cooled HOT side is currently at a lot higher temperature than our as of late warmed COLD side), the hotness is moved all the more effectively and the

surface region for our necessary hotness load is diminished. Assuming we are running a tight interaction and expected to cool extremely near our utility temperature, the LMTD would be tiny and accordingly require a lot of surface region to accomplish the ideal hotness move. One supposition for this relationship is that the particular hotness of our liquids stays consistent. On the off chance that we are searching for another hotness exchanger and are uncertain of what size we may be expecting, remember the LMTD we are giving it. The LMTD will by and large direct the number and style of plates inside the unit (length of the plate pack), while how much stream we wish to utilize will direct the port size required (tallness and Width).[8]

II. LITERATURE REVIEW

It worked for expanding Thermal Efficiency of a Counter Flow Air to Air Heat Exchanger. To fulfill the guidelines of uninvolved and low-energy houses, he limited the energy utilization of the warming framework. He in this way improved to recuperate however much hotness as could be expected from the exhaust air. Two hotness exchangers from REC Indovent Company were utilized for this work which was tried essentially with center around warm effectiveness. Estimations showed that the denser hotness exchanger returned a higher warm productivity, probable on the grounds that its bigger hotness move region. Tries additionally showed that the wind stream was unevenly dispersed through the exchanger on the exhaust side since the fan was put just before the hotness exchangers bay. Estimations showed that an even circulated wind current can work on the warm effectiveness. [9]

Air guides were utilized to coordinate the air all the more even and thus the warm proficiency was expanded. The advantages of utilizing air guides ended up being more particular for the first hotness exchanger than for the adjusted, since the last one showed a moderately decent wind stream circulation without utilizing any sort of air direction. This is presumably dependent on the way that the strain drop was bigger for the adjusted unit than for the first one and afterward functions as a diffuser. The utilization of air guides brought about an expansion of warm proficiency from 73.0% to 78.4% for a wind current of 55 l/s and from 74.6 to 81.0% for a wind stream of 86 l/s.[10]

It have chipped away at Advances in heat siphon frameworks. Their audit work extensively partitioned into three principle areas, starts with the different techniques for upgrading the exhibition of hotness siphons. This is trailed by an audit of the significant crossover heat siphon frameworks appropriate for application with different hotness sources. Ultimately, the paper presents novel uses of hotness siphon frameworks utilized in select ventures. Heat siphon frameworks offer efficient options of recuperating heat from various hotspots for use in different modern, business and private applications. As the expense of energy keeps on rising, it becomes basic to

save energy and further develop in general energy productivity. In this light, the hotness siphon turns into a critical part in an energy recuperation framework with incredible potential for energy saving. [11]

Further developing hotness siphon execution, unwavering quality, and its ecological effect has been a continuous concern. Late advances in heat siphon frameworks have trotted upon cutting edge cycle plans for both hotness and work-impelled frameworks, further developed cycle parts (counting decision of working liquid), and taking advantage of use in a more extensive scope of uses. For the hotness siphon to be an affordable recommendation, ceaseless endeavors should be committed to working on its exhibition and unwavering quality while finding novel applications. Some new exploration endeavors have particularly further developed the energy productivity of hotness siphon. For instance, the fuse of a hotness driven ejector to the hotness siphon has further developed framework productivity by over 20%. Furthermore, the advancement of better blower innovation can possibly diminish energy utilization of hotness siphon frameworks by as much as 80%.[12]

It was completed Performance Analysis of Primary Air Heater Under Particulate Condition in Lignite-Fired Power Plant. He concentrated on the presentation of cross-stream heat exchanger, known as the essential air radiator in a 300 MW lignite-terminated power plant under particulate, no spillage, and spillage conditions. Typically, this hardware trades heat between the hot vent gas and the channel burning air which works under a high substance of fly debris. Testing was executed with the full American culture of mechanical architects, execution test code no. 4.3 field test (ASME PTC 4.3) to give last confirmation of execution. The spillage upsides of chosen essential air warmer were 6.31, 7.37, and 7.65 % when the power plant was run at the producer ensured turbine generator limit of 100, 80, and 60 % separately. Under these conditions, the gas side proficiency of the chose essential air radiator was viewed as at the low degree of 66.83, 65.44, and 62.12 % and X-proportions were 0.92, 0.88, and 0.79 individually. The air radiator spillage and particulate matter affect the exhibition of essential air warmers and would keep an eye on helpless productivity.[13]

III. CONCLUSION

An attempt is made to recover the waste heat from air compressor plant used in industrial purpose. As indicated in this paper, the study provides the following conclusions:

- The study showed that the definite improvement in the COP of the refrigeration system.
- Thus the system efficiency is improved.
- The additional cost for the Heat Exchanger can be recovered by using the recycling system in the long run. Thus it leads to energy conservation. The system prevents condensation in air in the pneumatic pipeline.

References:

[1] P. Teertstra, M.M. Yovanovich, j.R. Culham, Analytical forced convection modeling of plate fin heat sinks,

j. Electron. Manuf. 10 (4) (2000) 253-261.

[2] Z. Duan, YS. Muzychka, Experimental investigation of heat transfer in impingement air cooled plate

fin heat sinks, ASME J. Electron. Packag. 128 (4) (2006) 412-418.

[3] E.M. Sparrow, D.S. Kadle, Effect of tip-to-shroud clearance on turbulent heat transfer from a shrouded,

longitudinal fin array, ASMEJ. Heat Transfer 108 (3)

(1986) 519-524.

[4] S.A. El-Sayed, S.M. Mohamed, A.M. Abdel-Itif, A.E. Abouda, Investigation of turbulent heat transfer and fluid

flow in longitudinal rectangular-fin arrays of different geometries and shrouded fin array, Exp, Therm. Fluid

Sci. 26 (8) (2002) 879-900.

[5] M. Saini, R.L. Webb, Heat rejection limits of air cooled plane fin heat sinks for computer cooling, IEEETrans.

Compon. Packag. Techno!. 26 (1) (2003) 71-79.

[6] R.j. Moffat, Modeling air-cooled heat sinks as heat exchangers, in: Proceedings of IEEE 23rd Semiconductor Thermal Measurement and Management Symposium, San jose, California, USA, 2007, pp. 200-207.

[7] A. Ortega, P. Skandakumaran, B. Hassell, A modified effectiveness-ntu approach for analysis of low aspect ratio mini-channel heat sinks using novel shape factor formulations, in: Proceedings of IEEE

Intersociety Conference on Thermal and Thermomechanical Phenomena in Electronic Systems, Orlando,

Florida, 2008, pp. 167-173.

[8] A. Bar-Cohen, I. Madhusudan, Design and optimization of air-cooled heat sinks for sustainable development,

IEEE Trans. Compon. Packag. Techno!. 25 (4) (2002) 584-591.

[9] P. Rodgers, V. Eveloy, M.G. Pecht, Limits of air-cooling: status and challenges, in: Proceedings of IEEE 21st

Semiconductor Thermal Measurement and Management Symposium, San jose, California, USA, 2005, pp. 116-

124.

[10] M. Toda, Theory of air flow generation by a resonant type PVF2 bimorph cantilever vibrator, Ferroelectrics

22 (1979) 911-918.